

Cost Elasticities of Reliability and *MTTF* for *k-out-of-n* Systems

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Abstract: The application of the concept of cost elasticity of reliability was extended from the parallel system to the partially redundant or *k-out-of-n:G(F)* system (or *k-out-of-n* system, for short). An expression for the cost elasticity of reliability was derived for a general *k-out-of-n* system. The expression yielded acceptable results for a wide range of values for *k*, *n*, and component reliability. For systems of practical interest characterized by good components, the expression became highly susceptible to round-off errors, and catastrophic cancellations took place. These numerical problems seemed unavoidable as they were inherently associated with the definition of the cost-elasticity-of-reliability metric itself. We introduced another metric, the cost elasticity of the Mean Time To Failure (*MTTF*), which measures the relative change in the life expectancy that can be obtained for a given relative change in cost. We believe the cost-elasticity-of-*MTTF* metric is a more tangible and a more cumulative measure than the cost-elasticity-of-reliability metric. We derived a very simple expression for the cost elasticity of *MTTF* for a *k-out-of-n* system and showed that it is a function of only *k* and *n*, i.e. it is independent of component characteristics such as component failure rate or component reliability. This expression is insensitive to round-off errors since it is a purely additive formula. We provided charts for the cost elasticity of *MTTF* that can be used to assess the cost incurred in achieving a certain life expectancy for a *k-out-of-n* system. These charts can be used with any coherent system, since the *MTTF* for a coherent system can be approximated by that of a *k-out-of-n* system.

Key words: Cost, Reliability, Mean time to failure, Parallel system, Partially redundant or *k-out-of-n:G(F)* system

INTRODUCTION

An important goal for reliability engineering is to achieve cost minimization [1]. However, this goal has rarely been achieved, primarily because of the lack of suitable mathematical models or metrics [2]. A recently introduced metric that captures the value of reliability from a financial viewpoint is the cost elasticity of reliability [3], defined as

$$\epsilon_{R,C} = (\Delta R / R) / (\Delta C / C). \quad (1)$$

This metric measures the relative change in reliability *R* that can be obtained for a given relative change in cost *C*. As its name indicates, this metric mimics a well-known material constant, viz., the modulus of elasticity which relates an applied stress to the resulting strain or relative change in length [4]. However, the metric $\epsilon_{R,C}$ is more analogous, from a cause-effect point of view, to

the price elasticity of demand or supply, a concept well known in microeconomics [5].

The new metric $\epsilon_{R,C}$ was studied in [3] in the case of a parallel system. We extend this study by applying this new metric to a *k-out-of-n:G(F)* system. The *k-out-of-n:G(F)* system is a system of *n* components that functions (fails) if at least *k* out of its *n* components function (fail). Situations in which this system serves as a useful model are frequently encountered in practice [6]. The *k-out-of-n* system plays a central role for the general class of coherent systems, as it can be used to approximate the reliability of such systems [7]. While virtually all nontrivial network reliability problems are known to be NP-hard for general networks, the regular structure of the *k-out-of-n* system allows the existence

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of efficient algorithms for its reliability analysis that are of quadratic-time linear-space complexity in the worst case [6]. The k -out-of- n :G system covers many interesting systems as special cases. These include the perfectly reliable system ($k = 0$), the parallel system ($k = 1$), the voting or N-modular redundancy (NMR) system ($k = \lceil (n + 1)/2 \rceil$), the fail-safe system ($k=n-1$), the series system ($k=n$), and the totally unreliable system ($k=n+1$). For $1 < k < n$ the k -out-of- n system is sometimes called a partially-redundant system [6], as it lies somewhere between the extreme cases of the (non-redundant) series system and the (fully-redundant) parallel system. The k -out-of- n :G system and the k -out-of- n :F system are mirror images of each other; their successes are dual switching functions. The k -out-of- n :G system is exactly equivalent to the $(n-k+1)$ -out-of- n :F system [6].

METHODOLOGY

The methodology adopted combines analysis and simulation. We derive an expression for $\epsilon_{R,C}$ for a parallel system based on the "continuous" limit $\Delta n \rightarrow 0$. We also derive an expression for $\epsilon_{R,C}$ for a general k -out-of- n :G system, but since it cannot be based on the continuous limit, we base it on what we call the best discrete increment $\Delta n = 1$, since this is the nearest possible increment to the continuous limit. We also introduce another metric, viz., $\epsilon_{T,C}$ or the cost elasticity of the *MTTF*, which we believe is a more tangible and a more accumulative measure than the $\epsilon_{R,C}$ metric. We derive a very simple expression for $\epsilon_{T,C}$ for a k -out-of- n :G system and show that it is a function of only k and n , i.e. it is independent of component characteristics such as component failure rate or component reliability. Furthermore, we present our experience and observations on computing $\epsilon_{R,C}$ and $\epsilon_{T,C}$.

Cost-reliability characterization for a parallel system: The unreliability of a parallel system with n identical but independent components of component reliability R_0 is given by:

$$1-R = (1-R_0)^n, \tag{2}$$

and hence, the reliability is given by:

$$R = 1 - (1 - R_0)^n. \tag{3}$$

Following Saleh et al. [3], we let the cost of a single component be C_0 , and assume that the cost of n components, C , scales linearly with the number of components, i.e.,

$$C = nC_0. \tag{4}$$

The change ΔR in reliability due to a change Δn in the number of components is:

$$\begin{aligned} \Delta R &= (\Delta R / \Delta n)\Delta n \approx (\partial R / \partial n)\Delta n \\ &= -(1 - R_0)^n \ln (1 - R_0) \Delta n, \\ &= (1-R_0)^n \ln \left(\frac{1}{1 - R_0} \right) \Delta n. \end{aligned} \tag{5}$$

The change in cost ΔC due to a change Δn in the number of components is

$$\Delta C = C_0 \Delta n. \tag{6}$$

Finally, the cost elasticity of reliability is given by

$$\epsilon_{R,C} = \frac{(1 - R_0)^n \ln \left(\frac{1}{1 - R_0} \right)}{[1 - (1 - R_0)^n]} n. \tag{7}$$

Equation (7) for $\epsilon_{R,C}$ is based on the use of

$$(\partial R / \partial n) = \lim_{\Delta n \rightarrow 0} (\Delta R / \Delta n),$$

i.e., it is obtained for the "continuous" limit $\Delta n \rightarrow 0$. Figure 1 shows a cost-reliability characterization of a parallel structure with n redundant components of a relatively good component reliability $R_0 = 0.9$. Figure 1(a) is a plot of unreliability ($1-R$) versus cost (expressed in units of C_0), which is essentially $(1-R)$, versus n , while Fig. 1(b) depicts cost elasticity of the structure's reliability versus n . Note that the system unreliability curve becomes quickly indistinguishable from the horizontal axis of value 0.

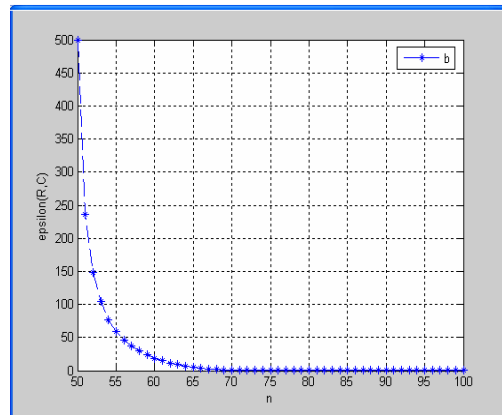
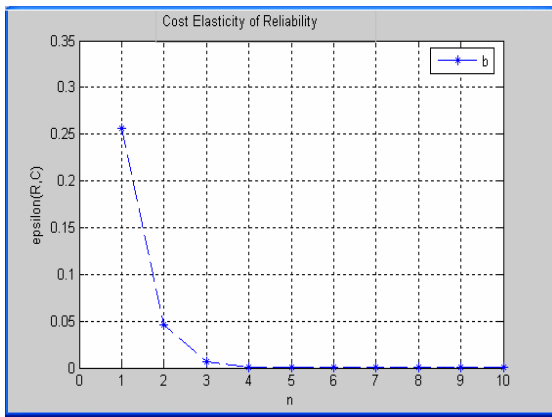
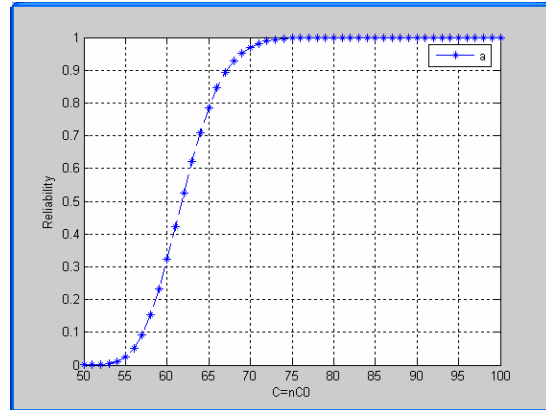
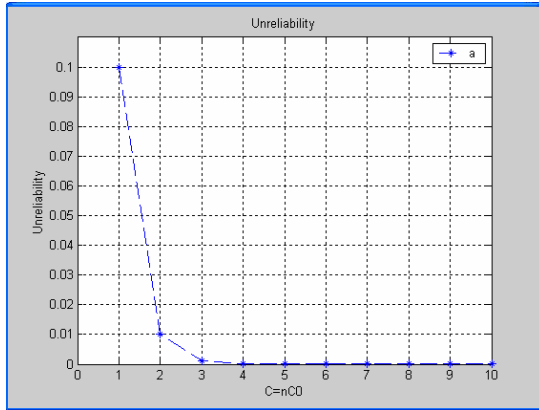


Fig.1: Cost-reliability characterization of a typical parallel structure

Fig. 2: Cost-reliability characterization of a 50-out-of- n :G system with component reliabilities $R_0 = 0.8$

Cost-reliability characterization for a k -out-of- n system: The reliability of a k -out-of- n :G system (with independent components of identical reliabilities R_0) is given by [6]:

$$R = \sum_{m=k}^n c(m,n) R_0^m (1 - R_0)^{n-m}, \quad (8a)$$

$$= \sum_{m=k}^n (-1)^{m-k} c(k-1, m-1) c(m,n) R_0^m, \quad (8b)$$

where $c(m,n)$ is the combinatorial or binomial coefficient (n choose m). If we let the number of components n change to $(n + \Delta n)$, then the reliability R in (8a) changes to $(R + \Delta R)$ given by

$$R + \Delta R = \sum_{m=k}^{n+\Delta n} \left(c(m, n + \Delta n) R_0^m (1 - R_0)^{n+\Delta n - m} \right). \quad (9)$$

From (8a) and (9), we can express the change ΔR in reliability due to a unit change $\Delta n=1$ in the number of components as

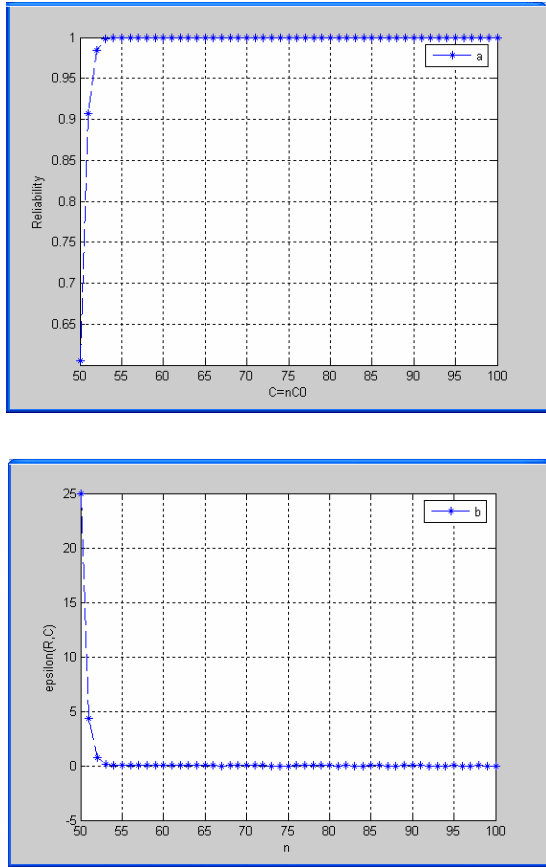


Fig. 3: Cost-reliability characterization of a 50-out-of- n :G system with component reliabilities $R_0 = 0.99$.

$$(\Delta R)_{\Delta n=1} = [c(n+1, n+1)R_0^{n+1} +$$

$$\sum_{m=k}^n (c(m, n+1)R_0^m(1-R_0)^{n+1-m} - c(m, n)R_0^m(1-R_0)^{n-m})]. \quad (10)$$

Using the binomial identifies

$$c(n+1, n+1) = 1, \quad (11)$$

$$c(m, n+1) - c(m, n) = c(m-1, n), \quad (12)$$

we reduce (10) to

$$(\Delta R)_{\Delta n=1} = R_0^{n+1} + \sum_{m=k}^n R_0^m(1-R_0)^{n-m} [c(m-1, n) - c(m, n+1)R_0], \quad (13)$$

and finally, obtain the cost elasticity of reliability as

$$\epsilon_{R,C} = \frac{n}{R} \left[R_0^{n+1} + \sum_{m=k}^n R_0^m(1-R_0)^{n-m} c(m-1, n) \left(1 - \frac{n+1}{m} R_0\right) \right]. \quad (14)$$

Formula (8a) is a purely additive formula; it expresses R as the sum of nonnegative terms. Formula (14) is not an additive formula unless $1 > \frac{n+1}{k} R_0$,

i.e., unless $R_0 < \frac{k}{n+1}$. Additive formulas have the

distinguishing characteristic that they are less prone to the inaccuracies (and never subject to the catastrophic cancellation) caused by round-off errors.

Figures 2 and 3 present a cost-reliability characterization for a 50-out-of- n :G system with component reliabilities $R_0 = 0.8$ and $R_0 = 0.99$, respectively.

Formula (14) for the cost elasticity of reliability $\epsilon_{R,C}$ gives satisfactory results up to $R_0 = 0.8$ (Fig. 2(b)) and then starts to exhibit some unacceptable negative values (values of -0 rather than +0), i.e. it exhibits erratic behavior for very small or negligible values of $\epsilon_{R,C}$ (Fig. 3(b)).

We must stress that the erratic behavior obtained is solely due to aggravated cumulative round-off error and is definitely not a result of some error in formulation or programming. Formula (14) gives acceptable and verifiable results for a wide range of values of k , n , and R_0 . However, it fails to assess $\epsilon_{R,C}$ properly for systems having good components (i.e., for systems of practical interest). Anyhow, for such systems $\epsilon_{R,C}$ diminishes and becomes indistinguishable from zero.

Equation (14) for $\epsilon_{R,C}$ is obtained by using the smallest possible nonzero discrete increment $\Delta n = 1$. This increment is the best discrete increment since it is the nearest one to the "continuous" limit $\Delta n \rightarrow 0$. For a parallel system ($k = 1$), we have two estimates for $\epsilon_{R,C}$, one based on the continuous limit $\Delta n \rightarrow 0$ in equation (7) and another based on the best discrete increment $\Delta n = 1$ in equation (14). Our computational experience reveals that there is no significant difference between these two estimates for large n , and small R_0 , i.e. when (14) is not spoiled by accumulated round-off errors.

Cost elasticity of *MTTF* for a k -out-of- n system:

From cost considerations, *MTTF* seems to be a more tangible and cumulative measure than reliability itself.

Therefore, we introduce the concept of the cost elasticity of the *MTTF*, which we define as

$$\epsilon_{T,C} = \frac{(\Delta T / T)}{(\Delta C / C)} = \frac{(\Delta T / T)}{(\Delta n / n)}, \quad (15)$$

where

$$T = MTTF = \int_0^{\infty} R(t) dt. \quad (16)$$

For a *k-out-of-n:G* system having components subject to a common constant failure rate (CFR) λ , the component reliability is

$$R_0(t) = e^{-\lambda t}, \quad t \geq 0, \quad (17)$$

and the *MTTF* of the system is obtained from equations (8b), (16), and (17) as

$$\begin{aligned} T &= \int_0^{\infty} \sum_{m=k}^n (-1)^{m-k} c(k-1, m-1) c(m, n) (e^{-\lambda t})^m dt, \\ &= \sum_{m=k}^n \frac{(-1)^{m-k}}{\lambda m} c(k-1, m-1) c(m, n). \end{aligned} \quad (18)$$

A simpler and a purely additive expression for *T*, however, can be obtained from the state diagram for a *k-out-of-n:G* system [8]. When the system is in state $m \geq k$, it has *m* working components and it behaves exactly as a series system of a failure rate $m\lambda$. The system resides in this state for an average time $(1 / (m\lambda))$, and hence the *MTTF* of the system is

$$T = \frac{1}{\lambda} \sum_{m=k}^n \frac{1}{m}. \quad (19)$$

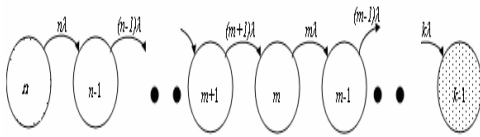


Fig. 4: State diagram for a *k-out-of-n:G* system, in which each state is indexed by the number of working components, and the shaded state (*k-1*) is one of catastrophic failure.

If we let the number of components *n* change to $(n + \Delta n)$ in (19), then the *MTTF* changes to $(T + \Delta T)$ given by

$$T + \Delta T = \frac{1}{\lambda} \sum_{m=k}^{n+\Delta n} \frac{1}{m}. \quad (20)$$

From (19) and (20), we can express the change ΔT in *MTTF* due to a unit change $\Delta n=1$ in the number of components as

$$(\Delta T)_{\Delta n=1} = \frac{1}{\lambda} \frac{1}{n+1}, \quad (21)$$

and hence, we can express $\epsilon_{T,C}$ as

$$\begin{aligned} \epsilon_{T,C} &= \frac{\frac{1}{\lambda} \frac{1}{n+1} n}{\frac{1}{\lambda} \sum_{m=k}^n \frac{1}{m}} = \frac{n}{n+1} \frac{1}{\sum_{m=k}^n \frac{1}{m}} \\ &= \frac{n}{n+1} \frac{1}{\frac{1}{k} + \frac{1}{k+1} + \dots + \frac{1}{n-1} + \frac{1}{n}}. \end{aligned} \quad (22)$$

The cost elasticity $\epsilon_{T,C}$ of the *MTTF* of a *k-out-of-n:G* system is a function of *n* and *k* only and is independent of the component reliability R_0 and the component failure rate λ .

Noting that the sum $S = \sum_{m=k}^n \frac{1}{m}$ satisfies the following inequalities for $k > 1$

$$S > \int_k^{n+1} \frac{dx}{x} = \ln\left(\frac{n+1}{k}\right), \quad (23)$$

$$S < \int_k^{n+1} \frac{dx}{x-1} = \ln\left(\frac{n}{k-1}\right), \quad (24)$$

we obtain the following tight bounds on $\epsilon_{T,C}$

$$\frac{n/(n+1)}{\ln\left(\frac{n}{k-1}\right)} < \epsilon_{T,C} < \frac{n/(n+1)}{\ln\left(\frac{n+1}{k}\right)}. \quad (25)$$

RESULTS

Table 1 lists $\epsilon_{T,C}$ values in proper-fraction form (exact integer arithmetic) for small k and n values. Figures 5 and 6 represent the cost elasticity of *MTTF* for a parallel system and for a 50-out-of- n :G system

Table 1: Value of $\epsilon_{T,C}$ as a function of k and n for $1 \leq k \leq n \leq 6$.

$\frac{n}{k}$	1	2	3	4	5	6
1	$\frac{1}{2}$	$\frac{4}{9}$	$\frac{9}{22}$	$\frac{48}{125}$	$\frac{50}{137}$	$\frac{120}{343}$
2		$\frac{4}{3}$	$\frac{9}{10}$	$\frac{48}{65}$	$\frac{50}{77}$	$\frac{120}{203}$
3			$\frac{9}{4}$	$\frac{48}{35}$	$\frac{50}{47}$	$\frac{120}{133}$
4				$\frac{16}{5}$	$\frac{50}{27}$	$\frac{360}{259}$
5					$\frac{25}{6}$	$\frac{180}{77}$
6						$\frac{36}{7}$

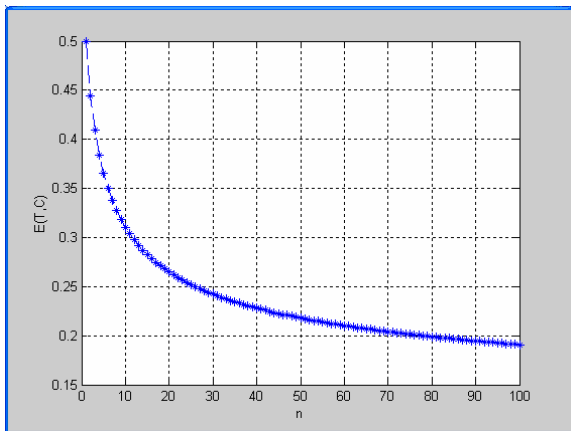


Fig. 5: Cost elasticity of *MTTF* for a parallel system versus its number of components n .

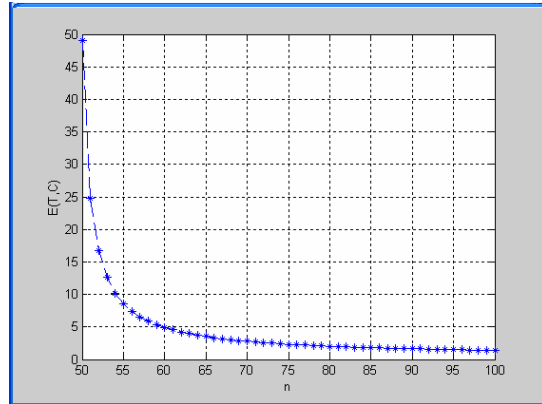


Fig. 6: Cost elasticity of *MTTF* for a 50-out-of- n :G system versus its number of components n .

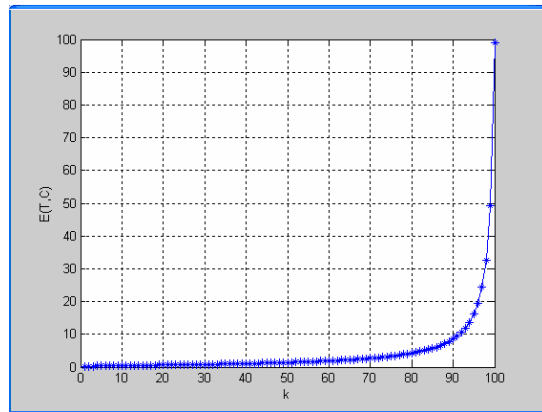


Fig. 7: Cost elasticity of *MTTF* for a k -out-of-100:G system versus the number of components k required for system success.

versus the number of components n . Figure 7 represents the cost elasticity of *MTTF* for a k -out-of-100:G system versus the number of components k required for system success. Table 1 and Figure 7 explain why the fail-safe ($(n-1)$ -out-of- n :G system or 2-out-of- n :F system) is so popular. Among redundancy systems it has the best cost for added redundancy since it has the highest $\epsilon_{T,C}$. Of course, the series system (n -out-of- n :G system or 1-out-of- n :F system) has an $\epsilon_{T,C} = (n^2/(n+1))$ that is higher than that of the fail-safe system, but the series system has no redundancy at all and cannot tolerate even a single failure.

DISCUSSION

The concept of cost elasticity of $MTTF \in_{T,C}$ introduced herein is a novel concept and has several advantages when compared with the earlier competitive concept of cost elasticity of reliability $\in_{R,C}$. One advantage stems from the fact that the $MTTF$ is a cumulative, integral, or averaging measure for reliability itself. For the wide class of k -out-of- n :G(F) systems $\in_{T,C}$ depends only on k and n while $\in_{R,C}$ depends on component characteristics in addition to its dependence on k and n . For such systems, it was possible to express $\in_{T,C}$ by a purely additive formula that is insensitive to round-off errors, while the $\in_{R,C}$ formula is very susceptible to round-off errors to the extent that catastrophic cancellations take place. Moreover, the $\in_{T,C}$ metric decreases but remains distinguishable from zero for large n , while the $\in_{R,C}$ metric diminishes and becomes indistinguishable from zero for large n and R_0 . This fact imposes a limitation on the utility of both metrics for large ultra-reliable systems.

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