

A Novel Architecture of Maximum Power Point Tracking for Ultra-Low-Power Based Hybrid Energy Harvester in Ubiquitous Devices: A Review

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ABSTRACT

This research work presents a novel architecture of an Ultra-Low-Power (ULP) based Hybrid Energy Harvester (HEH) consisting of multiple input sources such as kinetic, thermal and solar energy, harvested from passive human power. Having multiple ambient sources mitigates limitations caused by single sources especially for bodily-worn applications; however, this results in impedance mismatch among the different integrated sources. To overcome this limitation, the proposed ULP-HEH will use one power management unit with Maximum Power Point Tracking (MPPT) algorithm and impedance matching considerations to efficiently manage and combine power harvested from all three sources to achieve ULP consumptions. Among other crucial sub-modules of the ULP-HEH are its Asynchronous Finite State Machine (AFSM) cum resource sharing arbiter to prioritize and share energy sources for overall power reduction, an efficient rectification scheme for the piezoelectric input, an adaptive feedback for ULP conditioning, Zero-Current Switching (ZCS) for semi-lossless switching, a self-start circuit for low ambient startup, a Boost converter, a Buck regulator, a fuzzy-based micro-battery charger and a de-multiplexer to switch between harvesting or charging capabilities. All of which are implemented for maximum output extraction and minimal losses. This ULP-HEH will be developed in PSPICE software, Verilog coding under Mentor Graphics environment and later to be verified using Field Programmable Gate Array (FPGA) board before the final layout implementation in CMOS 0.13- μm process technology. This battery-less ULP-HEH is expected to deliver 3.0-5.0V of regulated voltage output from low ambient sources of 35 mV at startup. An efficiency of 90% with an output power of 650 μm is expected when all sources are summed. Also, this ULP-HEH is aimed at reducing power consumption to at least twice ($<70 \mu\text{W}$) of conventional approaches. The proposed ULP-HEH can be used for ULP bodily-worn electrical gadgets, wearable biomedical devices or to charge micro-batteries for portable electronic devices.

Keywords: Hybrid Energy Harvester (HEH), Ultra Low Power (ULP), Maximum Power Point Tracking (MPPT), Resource Sharing Arbiter, FPGA

1. INTRODUCTION

Energy harvesting dates back to the days of windmills, waterwheel and waste heat when batteries and dynamos were yet to be invented by (Khaligh and Onar,

2009) respectively. The recent accelerated interest in renewable energy harvesting is primarily motivated by an exponential increase in energy consumption, an inevitable future exhaustion of fossil fuel as well as negative ecological effects (Michaelides, 2012). Today,

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these renewable harvesting sources vary from solar, wind, thermal, ambient vibration, tidal wave, salinity gradient to the efficient reuse of exhaust heat discussed by (Yao *et al.*, 2009). Acknowledging this need, various harvesting technologies, topologies and power electronics interfaces for stand-alone utilization or grid connection application has surfaced (Ramadass and Chandrakasan, 2009; Khaligh and Onar, 2009; Hamilton, 2012). Some of them preceded with meso-scale energy harvesting systems and later followed by CMOS process implementation (Ramadass and Chandrakasan, 2009) with popular application varying from Wireless Sensor Networks (WSN) to the recently sprouted human powered devices of pacemakers (Zervos, 2013), shoe inserts harvesters (Rocha *et al.*, 2010) to a closed loop bio-medical monitoring system (Zhang *et al.*, 2010) fuels interests in the human harvesting arena.

This literature focuses on the Ultra-Low-Power (ULP) based Hybrid-Energy-Harvester (HEH) human powered applications which began ever since the invention of self-winding watch by Abraham-Louise Perrelet in the year 1770 (Bonfiglio and Rossi, 2011). There are essentially three plausible types of energy sources for wearable devices, namely the mechanical acceleration, electromagnetic light energy and heat flow identified by Bonfiglio and Rossi (2011). **Table 1** summarizes the energy harvesting opportunities and its demonstrated capabilities of these three energy sources (Vullers *et al.*, 2009). For these three energy sources, there is a difference between unobtrusive energy and the effort driven micro-power generation such as a shaken torch light, in which case the latter is rejected altogether for Body Area Networks (BAN) in biomedical applications (Bonfiglio and Rossi, 2011).

The following paragraphs describe vibration-based energy harvesters with its interface circuits, followed by thermoelectric-based harvesters with its management circuitries and related CMOS process implementation, succeeded by a discussion on Maximum Power Point Tracking (MPPT) techniques with solar related literatures and finally ending with the hybrid architectures, implemented die micrographs, author's hypothesis and a conclusion to gauge micro-energy harvesters' potential in human powered applications.

Firstly, there are three main types of vibration-based generators, namely electrostatic, electromagnetic and piezoelectric (Kempitiya *et al.*, 2012). These transducers became efficient with development of piezoelectric materials such as Lead Zirconate Titanate (PZT) and Polyvinylidene Fluoride (PVDF) (Rocha *et al.*, 2010), multiple PZT structures (Zhu *et al.*, 2011), encapsulated PZT nanofiber structure with 1.63 V of output voltage and 0.03 μW of output power (Chen *et al.*, 2010). Harvesting ambient vibration via PZT potentially supplies 10-100's μW of available power (Ramadass and Chandrakasan, 2009). Therefore, to complement these PZT structures, Rao and Arnold (2011) proposed an input-powered interface to solve the nonzero standby power consumption when no energy is harvested targeted at low amplitude output (0.1 V-5 V) and low frequency ac voltages of 1-500 Hz. Tabesh and Frechette (2010), designed an adaptive converter which optimally extracts power at 60% efficiency. Ramadass and Chandrakasan (2009), however reported 4-times improved power extraction via bias-flip rectification with lesser than 2 μW of power consumption.

Table 1. Energy harvesting opportunities and demonstrated capabilities (Vullers *et al.*, 2009)

Source	Characteristics	
	Source power	Harvester power
Solar		
Indoor	0.1 mW/cm ²	10 μW /cm ²
Outdoor	100 mW/cm ²	10mW/cm ²
Vibration		
Human	0.5m @ 1Hz 1 m/s @ 50 Hz	4 μW /cm ²
Industrial	1m @ 5Hz 10 m/s @ 1 kHz	1100 μW /cm ²
Thermal		
Human	20 mW/cm ²	30 μW /cm ²
Industrial	100 mW/cm ²	1-110mW/cm ²

On the other hand, D'hulst *et al.* (2010) suggests not to overlook converter's operating point by achieving 64% overall system efficiency while Aktata *et al.* (2011) uses rectifications with active diodes, shunt pass and a trickle charger to achieve power consumptions below 1 μ W with 50-60% efficiency compared to the architectures of Ramadass and Chandrakasan (2009) and Kwon and Rincon-Mora (2010) which requires initially charged batteries at 1.8 V and 2.5 V respectively.

Heat flow is another viable solution for low-powered bodily worn gadgets, where both sides of the Thermo Electric Generators (TEG) is attached to body and chips will only have temperature differences of 1-2°C thereby generating around 50 mV (Kim and Kim, 2012). Recent thermal harvesters addresses this commonly low voltage issue of 25-50 mV for body-worn applications (Carlson *et al.*, 2010; Ramadass and Chandrakasan, 2011; Im *et al.*, 2012; Richelli *et al.*, 2012). Carmo *et al.* (2010) fabricated a thermoelectric micro-converter based on thin films of bismuth and telluride to operate wireless electroencephalograms (EEG). Later, DC/DC Boosting techniques were used by Carlson *et al.* (2010), Ramadass and Chandrakasan (2011) and later by Richelli *et al.* (2012); Kim and Kim (2012) and Im *et al.* (2012) to increase efficiency of their power conditioning circuitries. Carlson *et al.* (2010) reported a control circuit that operates between 20 to 250 mV which produces a 1 V output from human body heat, consuming 1.6 μ W while delivering 25 μ W. Ramadass and Chandrakasan (2011) also reported another interface circuit targeted at human body heat implemented on 0.35 μ m CMOS process with a mechanical startup circuit at 58% efficiency which enables operation between 35 mV to 1.8 V. Richelli *et al.* (2012) on the other hand fabricated an 0.18 μ m low-threshold CMOS process which incorporates an architecture for boosting 120 mV to an output of 1.2 V, delivering 220 μ A to the load and exhibiting 30% power efficiency.

To design interface circuits for improved power extraction, Kim and Kim (2012) and Im *et al.* (2012) proposed an incorporation of the MPPT algorithm popularly used in solar harvesting (Kim *et al.*, 2011; Enne *et al.*, 2012) for above 70% efficiencies at 0.5 V to 2.7 V of input voltages. The former literature (Kim and Kim, 2012) presents a DC/DC boost converter with variation-tolerant MPPT algorithm for dynamic frequency switching and a highly efficient Zero Current Crossing (ZCS) control circuit for wide conversion ratios implemented on a 0.35- μ m bipolar-CMOS-DMOS (BCDMOS) process which outputs a 5.62 V from a 500mV supply at ~72% efficiency. Im *et al.* (2012) also reported usages of MPPT control on 0.13-

μ m CMOS process chip capable of providing 2.7 mW from 40mV to 300 mV supply with 61% efficiency at 2 V outputs where a transformer is self-started by thermal noise. This improved MPPT algorithm does not break the power transfer path and consumes less power (Im *et al.*, 2012).

A hybrid system combines multiple harvesting technologies into a single system to overcome energy shortfalls of separate systems. These systems are an attractive solution to sufficient power delivery over a wide range of environmental conditions and devices (Hamilton, 2012). Colomer *et al.* (2011) has reported a multi-harvesting system that gathers and manages energy from multiple sources to deliver ~6.4 mW of power on an Application Specific Integrated Circuit (ASIC) where each power source uses individual power management. Tan and Panda (2011), however reported a hybrid harvesting scheme that uses only one power management circuit alike Karthik *et al.* (2012) capable of 621 μ W of power generation, which triples single-source harvesting methods. Their chip was complemented by an efficient microcontroller based ULP management circuit, enhanced with MPPT with closed-loop voltage feedback control to ensure maximum power transfer (Tan and Panda, 2011). Another literature such as Karthik *et al.* (2012) also proposes one power management unit where the former reported > 80% charger efficiency (Karthik *et al.*, 2012) at 330 mV of kick-start voltage with clock gating and MPPT. **Table 2** summarizes some of these past researchers' work on hybrid energy harvesters.

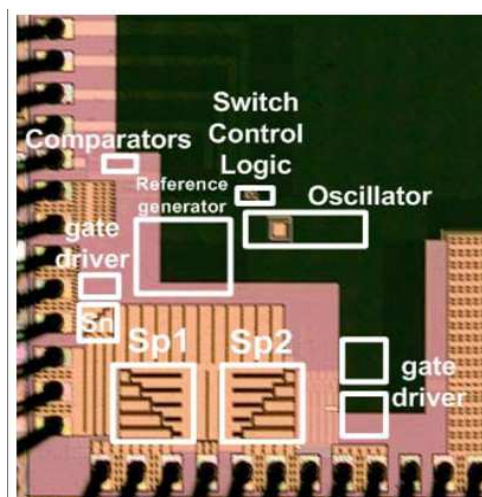


Fig. 1. Die micrograph of DIDO energy harvester for WBAN (Wang *et al.*, 2011)

Table 2. Past researcher works on hybrid energy harvesters

Researcher (Year)	Sources		Parameters		$V_{IN}(V)$	$V_{OUT}(V)$	P_{OUT}	η (%)	Power Used (W)	Process Technology	App. ^a (Is it dual usage?)
	(No.)	Architecture	MPPT	Kick-start scheme							
Tan and Panda (2011)	Light, Heat (2)	DC/DC converter, PWM gen., MCU	Yes	None	~3.6	~5.5	621 μ W	~90	135 μ W	H/W prototype	WSN (No)
Colomer <i>et al.</i> (2011)	RF, PZT, PV (3)	LDO regulator, charge pump, external SD	Yes	None	1 (RF), 1.2 (PZT), 1.89 (PV)	1.2-2.5	6.4 mW	55-85	160 μ W	ASIC 0.13 μ m	Low power loads, WSN (No)
Wang <i>et al.</i> (2011)	PV, TEG (2)	Switch Control Logic, Oscillator, DIDO Boost Converter	No	None	0.5	0.9-1	100 μ W	55	0.23 μ W	CMOS 0.18 μ m	WBAN (No)
Karthik <i>et al.</i> (2012)	PV, Heat (2)	Charger, FSM and oscillator, clock gating	Yes	Cold start (input powered Boost converter @ 0.33V)	0.5	3	Not stated	>80	330 nA of quiescent current	Fabricated IC	Battery and supercap. charger (No)
Porcarelli <i>et al.</i> (2012)	Air-flow, PV, Fuel Cell (3)	DC/DC in/ output converter charger, MCU	Yes	None	~3	Not stated	7~300mW	82-86	Not stated	Meso-scale 5 \times 6cm ² PCB	Li-ion battery charger (No)
Bandyopadhyay and Chandrakasan (2012)	PZT, Heat, PV(3)	Dual Path Approach, inductor sharing	Yes	None	0.02-0.16 (Heat) 0.15-0.75(PV) 1.5-5 (PZT)	1.88-2.3	1.3 mW (Heat) 2.5 mW (PV) 200 μ W (PZT)	58% (Heat) 83% (PV) 79% (PZT)	Not stated	CMOS 0.35 μ m	DSPs, sensors (No)
Sang <i>et al.</i> (2012)	EM, PZT (2)	Full bridge rectifier	No	Electro- dynamic Shaker	Not stated	0.71	10.7 mW	*81.4 %	Not stated > single source EM	Meso-scale prototype	WSN (No)
Michelle <i>et al.</i> (2013)	PZT, Heat, PV (3)	Resource sharing Arbiter, AFSM, ULP f/b, fuzzy charger, DC/DC converter, ZCS	Yes	Self start switch/ power supply manager @~35mV	0.1-0.3	3.0-5.0	> 650 μ W	>90	<70 μ W	CMOS 0.13 μ m	Body worn devices cum charger (Yes)

a. Application.

As an example, three of the literatures Wang *et al.* (2011); Karthik *et al.* (2012) and Bandyopadhyay and Chandrakasan (2012) from **Table 2** have fabricated and reported their die micrographs with Wang *et al.* (2011) die as shown in **Fig. 1** bearing the closest resemblance to the proposed ULP based HEH because of its similar input sources and single power management unit. This literature focuses on Dual-Input Dual-Output (DIDO) Boost conversion for Wireless Body Area Network (WBAN) fabricated on a 0.18- μ m CMOS process technology which occupies a die area of 1160 \times 1000 μ m. The hybrid inputs are solar (M5525-0.5V) and heat (MPG-D651 TEG) with minimum input voltages of 0.5 V and very low power consumption of 0.23 μ W with 55% efficiency (Wang *et al.*, 2011). The die of this DIDO harvester shows the placements of the adaptive frequency ring oscillator, gate driver, switch control logic, reference generator sub-blocks which constitute some main portion of its entire power conditioning architecture.

This literature survey shows profound interest in micro-energy harvesting for ULP devices. However, there is still a lack of low cost universal solution to battery or fossil power replacement as implementation of technology is application dependent, thereby one size does not suit all needs. Also, there is the concern of alternative energy efficiency, where in the case of a low cost crystalline silicon solar cell module, the efficiency barely reaches 20% (Gassenbauer *et al.*, 2013). This is where advanced circuit technology comes in by introducing almost lossless rectifications (Ramadass and Chandrakasan, 2009), power boosting circuitries by Carlson *et al.* (2010); Ramadass and Chandrakasan (2011); Richelli *et al.* (2012) and Kim and Kim (2012), timing controls (Kim and Kim, 2012), closed loop schemes (Zhang *et al.*, 2010), MPPT algorithms (Im *et al.*, 2012; Kim and Kim, 2012), as well as dual paths and inductor sharing schemes (Bandyopadhyay and Chandrakasan, 2012) in which the author has given a hypothesis on the contribution in this arena with the proposed ULP based HEH's specifications as summarized in **Table 2** previously.

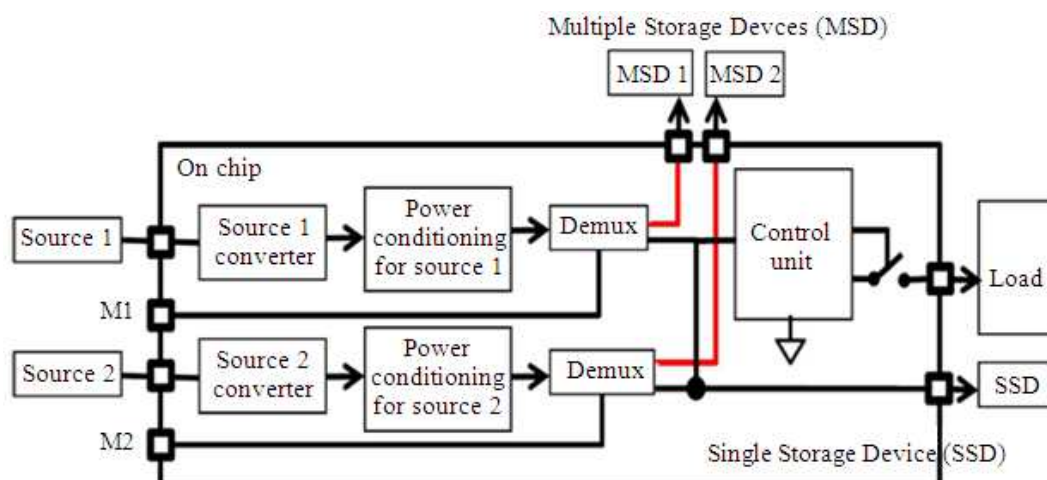


Fig. 2. Conventional architecture of HEH source with separate power management circuitries (Colomer *et al.*, 2011)

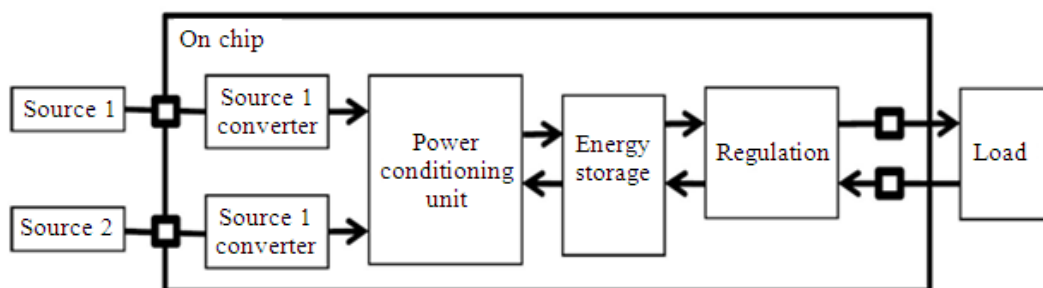


Fig. 3. Conventional architecture of HEH source with single power management circuitries (Tan and Panda, 2011; Sarpeshkar, 2010)

Therefore, the author proposes 3 input sources from solar, heat and vibration to be implemented on 0.13- μm CMOS process technology with self-start mechanism, resource sharing capabilities, state machine, fuzzy-based charging, Buck and Boost converters with MPPTs. which is expected to obtain hypothetical output voltages of 3.0-5.0 V at more than 90% efficiency with below 70 μW of power consumption and a V_{IN} of 100 to 300 mV at an operating frequency of 4kHz.

In a nutshell, to anticipate the energy crunching society that we are to become, energy harvesting technology and techniques has been rapidly advancing in the past few years. Significant efforts has been put forth to address limitations in the micro-scale energy harvesting arena. One substantial need is a robust, energy efficient harvester for ubiquitous devices, a hybrid harvesting device looks promising to overcome shortfalls of individual sources especially for delivering power to a much wider range of environment.

1.1. Statement of Problem

The purpose of this research is to address the problem faced by past researchers in most body-worn energy harvesters which suffers from low conversion ratios due to relatively low ambient input. Here, two conventional HEH topologies are given in **Fig. 2** and **3**. **Figure 2** shows a conventional block diagram of an HEH with individual power conditioning circuitry for each individual source (Colomer *et al.*, 2011). Sources can either be summed together or utilized separately (Colomer *et al.*, 2011). This approach increases cost, form factor, power losses and requires external storage devices. **Figure 3** represents another conventional HEH architecture with an improvement over **Fig. 2**. It shares a single power conditioning unit with built in energy storage such as the design proposed by Wang *et al.* (2011) and Tan and Panda (2011). The architecture in **Fig. 3** improves the topology of **Fig. 2** by form factor, cost and power losses as only one set of power management circuit is used.

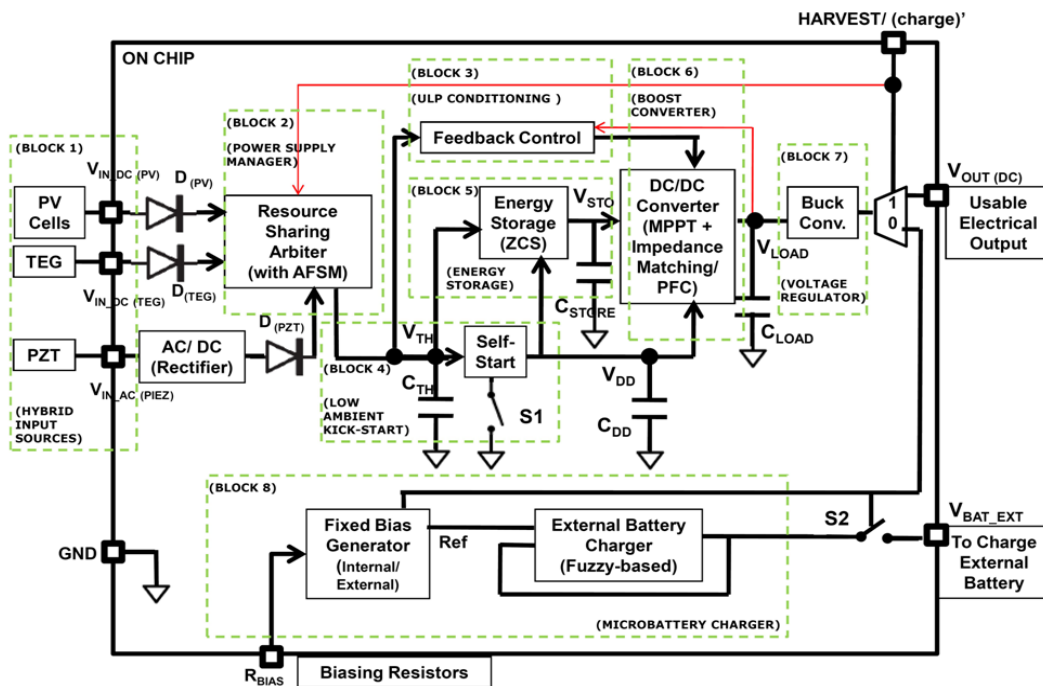


Fig. 4. Proposed architecture of the ULP based HEH for ubiquitous devices

However, the challenge is the possibility of impedance mismatching issue among the integrated energy sources (Tan and Panda, 2011).

The proposed solution to resolve the drawback of a single energy source is an HEH capable of converting sunlight, body heat and mechanical movement into electrical signals. Therefore, the proposed HEH system will have three input sources from the Photovoltaic (PV), TEG and PZT sources capable of combined or individual conditioning of harvested sources. On the other hand, this study also proposes a DC/DC converter which incorporates impedance matching and power factor correction considerations into its developed MPPT algorithm to address the multi-source impedance mismatch issue. Another challenge would be enabling the HEH system to consume as low power as possible; this is achieved with an adaptive low power conditioning feedback control loop, motivated by Rao and Arnold (2011). The proposed feedback loop will maintain the open circuit Voltage (V_{oc}) of the HEH system by adjusting the duty cycle of the DC/DC Converter. It will also detect the absence of input energy and eliminate standby power consumption (Rao and Arnold, 2011).

Most HEH systems are either energy harvesters (Colomer *et al.*, 2011; Tan and Panda, 2011) or external micro-battery chargers (Khosropour *et al.*, 2012). This

study propose to combine both the harvesting and charging ability of an HEH with possibly fuzzy logic implementation (Huang *et al.*, 2009) which will potentially be integrated into the DC/DC buck charger of its harvester function to lower the overall form factor. The proposed ULP based HEH system uses no battery and in case of an ultra low ambient condition, has a self-start circuit capable of kick-starting from a light human motion similar to that in (Ramadass and Chandrakasan, 2011). Above all, the proposed ULP based HEH architecture will be implemented on a 0.13- μm CMOS process technology similar to the HEH conditioning interface circuit to extract maximum power found in Colomer *et al.* (2011). Finally, the purpose here is to investigate the best power conditioning interface circuit to extract maximum power and dissipate minimum losses.

1.2. Description (Proposed Block)

The proposed ULP based HEH architecture is shown in Fig. 4. It consists of eight sub-blocks i.e., (Block 1, Block 2, ... Block 8) which represents the hybrid input sources, power supply manager, ULP conditioning circuitry, low-ambient kick-starter, energy storage, Boost converter with MPPT, Buck regulator and battery charger blocks respectively. All eight blocks will work together to address a few main challenging issues. These

blocks will be subsequently explained by the following paragraphs here forth.

Firstly, the hybrid input sources such as PV, TEG and PZT (Block 1) are applied to the ULP based HEH. These sources represent the multi-ambient source for body-worn devices applicable both outdoors under the sun and indoors with heat gradients or kinetic movement by the body to mitigate a possible absence of either one source. These sources are capable of powering up body worn devices to a multitude of voltage levels. The proposed ULP-HEH architecture captures solar power, human temperature gradient and vibration from the ambient environment via a PV Cell, TEG and PZT respectively. Only the PZT source which is a small signal alternating current requires efficient rectification from voltage doublers (Tabesh and Frechette, 2010), shunt pass switches (Aktata *et al.*, 2011) to bias-flip chip methods (Ramadass and Chandrakasan, 2009) which achieves 4-times better power extraction than conventional full bridge rectifiers. All three DC sources from the transducers are individually fed into diodes to avoid reverse current flow (Tan and Panda, 2011).

Secondly, these three hybrid input sources will then be fed into the power supply manager (Block 2) with resource sharing arbiter and an Asynchronous Finite State Machine (AFSM) to efficiently share resources and manage individual or summation of power supplies inspired by Ramadass and Chandrakasan (2009) and Colomer *et al.* (2011). The AFSM integrated into this block will decide between one of the four options which are: (i) to manage priority between the three sources when they are simultaneously present (Tan and Panda, 2011; Bandyopadhyay and Chandrakasan, 2012), (ii) to decide between harvesting external loads or charging an external battery based on the user selection feedback aided by a simple multiplexer. (iii) to activate "Request/Acknowledgement" signals between shared resources such as an inductor sharing request suggested by Ramadass and Chandrakasan (2009) or a possibility of bidirectional DC/DC conversion of "reverse-buck forward-boost" approach suggested by Arfin and Sarpeshkar (2012) in their energy efficient electrode stimulator, (iv) to trigger self-starting or energy recycling such as the inductor-based scheme to recycle energy between positive and negative phases reported by Kim and Kim (2012); Tan and Panda (2011) as well as Arfin and Sarpeshkar (2012).

Thirdly, the ULP feedback conditioning control (Block 3) is used to adaptively adjust duty cycle of DC/DC converter based on feedback to ensure that V_{OUT} is stable and reduce power losses to its minimum motivated by Rao and Arnold (2011). It ensures ULP is

consumed throughout the entire harvesting process. It maintains a stable open circuit voltage, V_{OC} as well as adjusts duty cycle of the DC/DC Boost converter based on the driven load similar to the analog controller introduced by Tabesh and Frechette (2010). It also eliminates standby power consumption by automatically shutting down the ULP based HEH when the ambient inputs are too low for successful harvesting such as the input-powered AC/DC converter suggested by Rao and Arnold (2011).

Next, the low ambient kick-start block (Block 4) houses switch S1 acts much like the one by Ramadass and Chandrakasan (2011) which is included as a fail-safe block to ensure that an internal storage element starts charging once one or more ambient sources is detected and also to eliminate battery-startup dependencies such as those reported by Aktata *et al.* (2011). The self-start mechanism charges C_{DD} to a minimal voltage value which will then trigger an internal clock within the self-start block which then triggers CMOS switches to help pump in further charge into C_{DD} to a proposed 2 V or above such as the one reported by Ramadass and Chandrakasan (2011).

Once the V_{DD} reaches this voltage level, the energy storage block (Block 5) with ZCS for semi-lossless switching (Kim and Kim, 2012) is activated and energy is stored in a storage capacitor, C_{STORE} which is designed to be much larger than C_{DD} (Ramadass and Chandrakasan, 2009; 2011; Aktata *et al.*, 2011). C_{STORE} will act as a buffer for this HEH system to ensure non-intermittent power supply and it can be used later on when no ambient sources are detected. Both V_{DD} and V_{STORE} cannot be used to directly power loads as C_{DD} will be designed to be small to maximize the net low voltage startup value after consideration of losses (Ramadass and Chandrakasan, 2011). Although the power is diverted into a much larger C_{STORE} after a proposed 2 V value has been reached, V_{STORE} is unstable and dependent on ambient input power available as well as the power consumed by the load (Tabesh and Frechette, 2010; Ramadass and Chandrakasan, 2011; Kim and Kim, 2012; Tan and Panda, 2011).

Thus, V_{STORE} needs to be boosted by a Boost converter block (Block 6) where a developed MPPT algorithm (Im *et al.*, 2012; Kim and Kim, 2012) is used to enhance power extraction while impedance matching is also incorporated to counteract the possibility of impedance mismatch caused by multiple power sources. Once boosted, the buck converter (Block 7) will regulate the V_{STORE} to a constant voltage value to power load circuits. Here, the MPPT, impedance matching and Power Factor Correction (PFC) is incorporated into the buck and boost converters to improve the ULP-HEH system's efficiency as well as impedance mismatches.

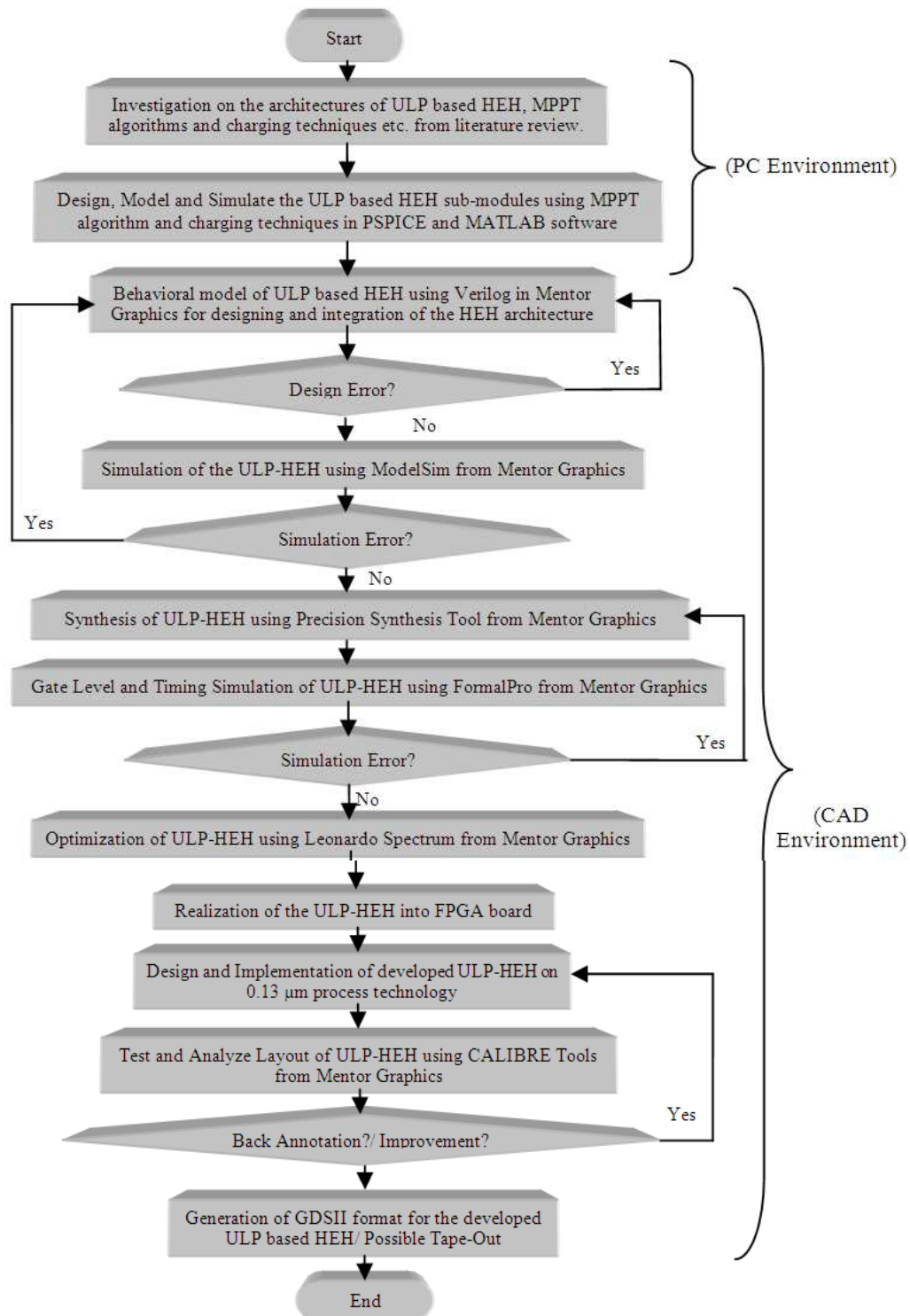


Fig. 5. Design flow chart of ULP based HEH architecture in PC and CAD environments

Finally, this ULP-HEH has a micro-battery charger (Block 8) with the ability to provide Li-ion battery charging on top of operating as a power source harvesting for bodily worn devices. Externally through a de-multiplexer, if the charging of external batteries were activated via the HARVEST/(charge)' terminal, external Lithium ion batteries can be charged with either an internal biasing circuit inspired by Khosropour *et al.* (2012) and Valle *et al.* (2011) or an externally configured bias much like the solar/thermal charger proposed in Karthik *et al.* (2012) instead of functioning as a harvester. The proposed battery charger has its own fuzzy based feedback control to monitor external battery charging status similar to those reported by Carlson *et al.* (2010) and Valle *et al.* (2011). Therefore, with these eight sub-blocks efficiently integrated, the novel ULP based HEH architecture, implemented in 0.13- μm CMOS technology, with 100-300 mV of input voltages from three ambient energy harvesting sources will be expected to deliver up to 3.0-5.0 V of output voltage which will be higher than past researchers of similar implementation platform, an efficiency above 90% and above 650 μW of output power with merely 35 mV of low kick-start value and below 70 μW of power consumption as well as the additional ability to charge external Li-ion batteries up to 3.0-5.0 V.

1.3. Implementation Process of HEH Architecture (Method)

The design flow chart for the proposed ULP based HEH is as shown in Fig. 5 where it will start with an exhaustive literature review and end with the generation of tape-out ready GDSII format. This implementation process will be sequentially discussed using the following sub-blocks.

The process flow for this ULP based HEH is implemented in the PC environment and CAD environment. Firstly, in the PC environment, a review on the architectures of ULP based HEH architectures, MPPT algorithms and charging techniques. will be investigated. Next, each sub-modules of the ULP based HEH will be modeled, designed and simulated in the PSPICE software. On the other hand, MATLAB will be used for MPPT algorithms and fuzzy-based charging techniques. Here, the desired kick-start voltage as low as ≤ 35 mV will be attempted. Any undesirable or erroneous simulation results especially regarding efficiency, power consumption, input and output voltages will be propagated back to the design or literature level. A successful simulation will lead to the design and integration of the ULP-HEH behavioral model written in

Verilog using Mentor Graphics which will be performed in the CAD environment together with all remaining tasks. This HDL based design of ULP-HEH will be simulated in the ModelSim and any discrepancies in design or simulation at this stage will lead back to the redesigning stage. Next, the behavioral model of ULP-HEH will be synthesized using the Precision Synthesis tool to enable a gate level simulation in the FormalPro tool. Any gate-level simulation faults will lead back to the synthesis stage.

An optimum gate-level synthesis will lead to the optimization of the gate-level ULP based HEH based on area, performance and power using the Leonardo Spectrum tool. If no further optimization is required, the optimized architecture will then be realized on the ULP-HEH architecture and lead to the realization of ULP-HEH by downloading into the Field Programmable Gate Array (FPGA) board as the target technology. With this successful FPGA implementation, the developed ULP-HEH will then be designed and implemented as transistor level model on the 0.13 μm process technology using Mentor Graphic's DA and IC station to obtain its final layout. Once the ULP-HEH layout is completed, testing and analysis will be conducted on the ULP-HEH layout and a series of tests will be done by CALIBRE to verify whether or not an improvement or back annotation is required before the final implementation especially if the ULP-HEH system has discrepancies in terms of parasitic, timing or power issues. After CALIBRE's verification on the ULP-HEH layout, the tape-out ready GDSII format can finally be generated to possibly be fabricated for real-life usages and validated for ubiquitous devices with human as ambient input sources.

2. CONCLUSION

A near optimal dual-functional ULP based HEH architecture has been proposed with both battery-charging and harvesting options. The main aim is to maximize the extracted input and minimize the power losses obtained from piezoelectric, photovoltaic and thermoelectric harvesters. This will be achieved by using an AFSM, a kick-start block, MPPT algorithm, impedance matching and feedback circuitry, ZCS as well as resource sharing approach to minimize losses throughout the ULP-HEH architecture. The proposed ULP-HEH architecture will be modeled, designed and simulated in PSPICE software, with MPPT and battery charging algorithm performed in MATLAB. The designed ULP-HEH will then realized on an FPGA and the layout verified in the 0.13- μm CMOS process technology in Mentor Graphics environment. Finally, the

expected result is to achieve a power reduction of at least 2-times ($<70\mu\text{W}$) conventional HEH with at least a 3.0-5.0 V regulated output at 4 kHz operating frequency, 90% efficiency and a power of about $650\mu\text{W}$ when all three sources are simultaneously harvested which has the ability to constantly power or charge any low power wearable devices.

3. REFERENCES

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