

## Cost Elasticities of Reliability and *MTTF* for *k*-out-of-*n* Systems

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**Abstract:** The application of the concept of cost elasticity of reliability was extended from the parallel system to the partially redundant or *k*-out-of-*n*:G(F) system (or *k*-out-of-*n* system, for short). An expression for the cost elasticity of reliability was derived for a general *k*-out-of-*n* system. The expression yielded acceptable results for a wide range of values for *k*, *n*, and component reliability. For systems of practical interest characterized by good components, the expression became highly susceptible to round-off errors, and catastrophic cancellations took place. These numerical problems seemed unavoidable as they were inherently associated with the definition of the cost-elasticity-of-reliability metric itself. We introduced another metric, the cost elasticity of the Mean Time To Failure (*MTTF*), which measures the relative change in the life expectancy that can be obtained for a given relative change in cost. We believe the cost-elasticity-of-*MTTF* metric is a more tangible and a more cumulative measure than the cost-elasticity-of-reliability metric. We derived a very simple expression for the cost elasticity of *MTTF* for a *k*-out-of-*n* system and showed that it is a function of only *k* and *n*, i.e. it is independent of component characteristics such as component failure rate or component reliability. This expression is insensitive to round-off errors since it is a purely additive formula. We provided charts for the cost elasticity of *MTTF* that can be used to assess the cost incurred in achieving a certain life expectancy for a *k*-out-of-*n* system. These charts can be used with any coherent system, since the *MTTF* for a coherent system can be approximated by that of a *k*-out-of-*n* system.

**Key words:** Cost, Reliability, Mean time to failure, Parallel system, Partially redundant or *k*-out-of-*n*:G(F) system

## INTRODUCTION

An important goal for reliability engineering is to achieve cost minimization [1]. However, this goal has rarely been achieved, primarily because of the lack of suitable mathematical models or metrics [2]. A recently introduced metric that captures the value of reliability from a financial viewpoint is the cost elasticity of reliability [3], defined as

$$\epsilon_{R,C} = (\Delta R / R) / (\Delta C / C). \quad (1)$$

This metric measures the relative change in reliability *R* that can be obtained for a given relative change in cost *C*. As its name indicates, this metric mimics a well-known material constant, viz., the modulus of elasticity which relates an applied stress to the resulting strain or relative change in length [4]. However, the metric  $\epsilon_{R,C}$  is more analogous, from a cause-effect point of view, to

the price elasticity of demand or supply, a concept well known in microeconomics [5].

The new metric  $\epsilon_{R,C}$  was studied in [3] in the case of a parallel system. We extend this study by applying this new metric to a *k*-out-of-*n*:G(F) system. The *k*-out-of-*n*:G(F) system is a system of *n* components that functions (fails) if at least *k* out of its *n* components function (fail). Situations in which this system serves as a useful model are frequently encountered in practice [6]. The *k*-out-of-*n* system plays a central role for the general class of coherent systems, as it can be used to approximate the reliability of such systems [7]. While virtually all nontrivial network reliability problems are known to be NP-hard for general networks, the regular structure of the *k*-out-of-*n* system allows the existence

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of efficient algorithms for its reliability analysis that are of quadratic-time linear-space complexity in the worst case [6]. The  $k$ -out-of- $n$ :G system covers many interesting systems as special cases. These include the perfectly reliable system ( $k = 0$ ), the parallel system ( $k = 1$ ), the voting or N-modular redundancy (NMR) system ( $k = \lceil (n+1)/2 \rceil$ ), the fail-safe system ( $k=n-1$ ), the series system ( $k=n$ ), and the totally unreliable system ( $k=n+1$ ). For  $1 < k < n$  the  $k$ -out-of- $n$  system is sometimes called a partially-redundant system [6], as it lies somewhere between the extreme cases of the (non-redundant) series system and the (fully-redundant) parallel system. The  $k$ -out-of- $n$ :G system and the  $k$ -out-of- $n$ :F system are mirror images of each other; their successes are dual switching functions. The  $k$ -out-of- $n$ :G system is exactly equivalent to the  $(n-k+1)$ -out-of- $n$ :F system [6].

## METHODOLOGY

The methodology adopted combines analysis and simulation. We derive an expression for  $\epsilon_{R,C}$  for a parallel system based on the "continuous" limit  $\Delta n \rightarrow 0$ . We also derive an expression for  $\epsilon_{R,C}$  for a general  $k$ -out-of- $n$ :G system, but since it cannot be based on the continuous limit, we base it on what we call the best discrete increment  $\Delta n = 1$ , since this is the nearest possible increment to the continuous limit. We also introduce another metric, viz.,  $\epsilon_{T,C}$  or the cost elasticity of the MTTF, which we believe is a more tangible and a more accumulative measure than the  $\epsilon_{R,C}$  metric. We derive a very simple expression for  $\epsilon_{T,C}$  for a  $k$ -out-of- $n$ :G system and show that it is a function of only  $k$  and  $n$ , i.e. it is independent of component characteristics such as component failure rate or component reliability. Furthermore, we present our experience and observations on computing  $\epsilon_{R,C}$  and  $\epsilon_{T,C}$ .

**Cost-reliability characterization for a parallel system:** The unreliability of a parallel system with  $n$  identical but independent components of component reliability  $R_0$  is given by:

$$1-R = (1-R_0)^n, \quad (2)$$

and hence, the reliability is given by:

$$R = 1 - (1 - R_0)^n. \quad (3)$$

Following Saleh et al. [3], we let the cost of a single component be  $C_0$ , and assume that the cost of  $n$  components,  $C$ , scales linearly with the number of components, i.e.,

$$C = nC_0. \quad (4)$$

The change  $\Delta R$  in reliability due to a change  $\Delta n$  in the number of components is:

$$\Delta R = (\Delta R / \Delta n) \Delta n \approx (\partial R / \partial n) \Delta n$$

$$= - (1 - R_0)^n \ln(1 - R_0) \Delta n, \\ = (1 - R_0)^n \ln\left(\frac{1}{1 - R_0}\right) \Delta n. \quad (5)$$

The change in cost  $\Delta C$  due to a change  $\Delta n$  in the number of components is

$$\Delta C = C_0 \Delta n. \quad (6)$$

Finally, the cost elasticity of reliability is given by

$$\epsilon_{R,C} = \frac{(1 - R_0)^n \ln \frac{1}{(1 - R_0)}}{[1 - (1 - R_0)^n]} n. \quad (7)$$

Equation (7) for  $\epsilon_{R,C}$  is based on the use of

$$(\partial R / \partial n) = \lim_{\Delta n \rightarrow 0} (\Delta R / \Delta n),$$

i.e., it is obtained for the "continuous" limit  $\Delta n \rightarrow 0$ . Figure 1 shows a cost-reliability characterization of a parallel structure with  $n$  redundant components of a relatively good component reliability  $R_0 = 0.9$ . Figure 1(a) is a plot of unreliability ( $1-R$ ) versus cost (expressed in units of  $C_0$ ), which is essentially  $(1-R)$ , versus  $n$ , while Fig. 1(b) depicts cost elasticity of the structure's reliability versus  $n$ . Note that the system unreliability curve becomes quickly indistinguishable from the horizontal axis of value 0.

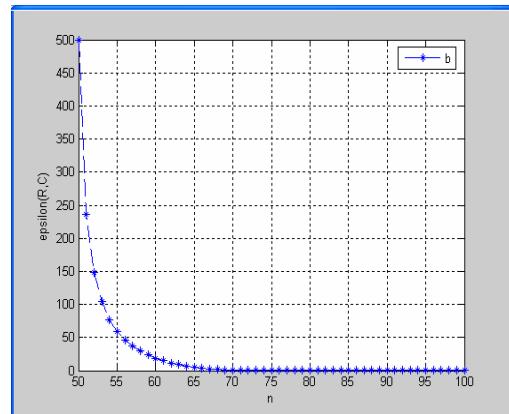
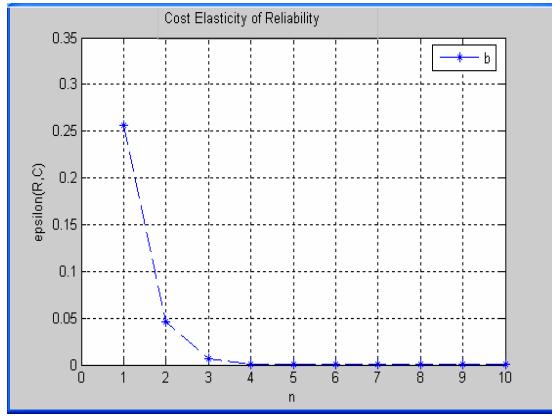
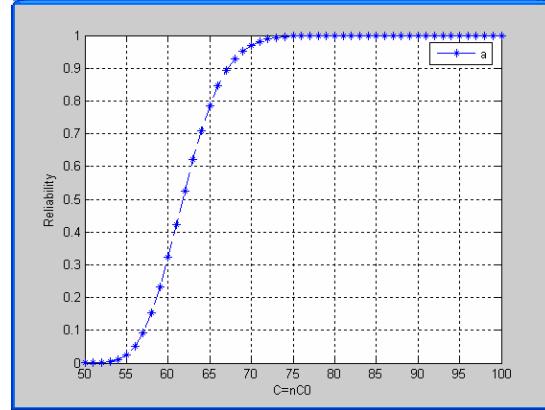
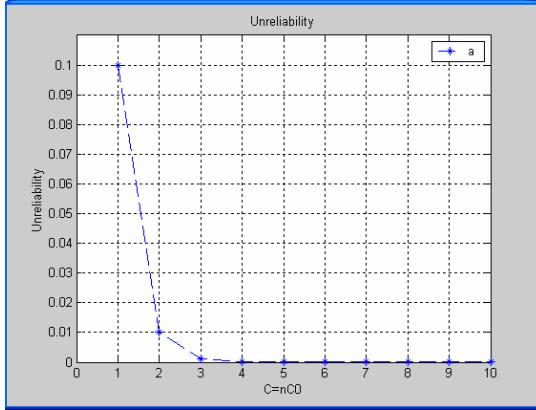


Fig.1: Cost-reliability characterization of a typical parallel structure

**Cost-reliability characterization for a  $k$ -out-of- $n$  system:** The reliability of a  $k$ -out-of- $n$ :G system (with independent components of identical reliabilities  $R_0$ ) is given by [6]:

$$R = \sum_{m=k}^n c(m,n) R_0^m (1-R_0)^{n-m}, \quad (8a)$$

$$= \sum_{m=k}^n (-1)^{m-k} c(k-1, m-1) c(m, n) R_0^m, \quad (8b)$$

Fig. 2: Cost-reliability characterization of a 50-out-of- $n$ :G system with component reliabilities  $R_0 = 0.8$

where  $c(m,n)$  is the combinatorial or binomial coefficient ( $n$  choose  $m$ ). If we let the number of components  $n$  change to  $(n + \Delta n)$ , then the reliability  $R$  in (8a) changes to  $(R + \Delta R)$  given by

$$R + \Delta R = \sum_{m=k}^{n+\Delta n} \left( c(m, n + \Delta n) R_0^m (1 - R_0)^{n+\Delta n - m} \right). \quad (9)$$

From (8a) and (9), we can express the change  $\Delta R$  in reliability due to a unit change  $\Delta n=1$  in the number of components as

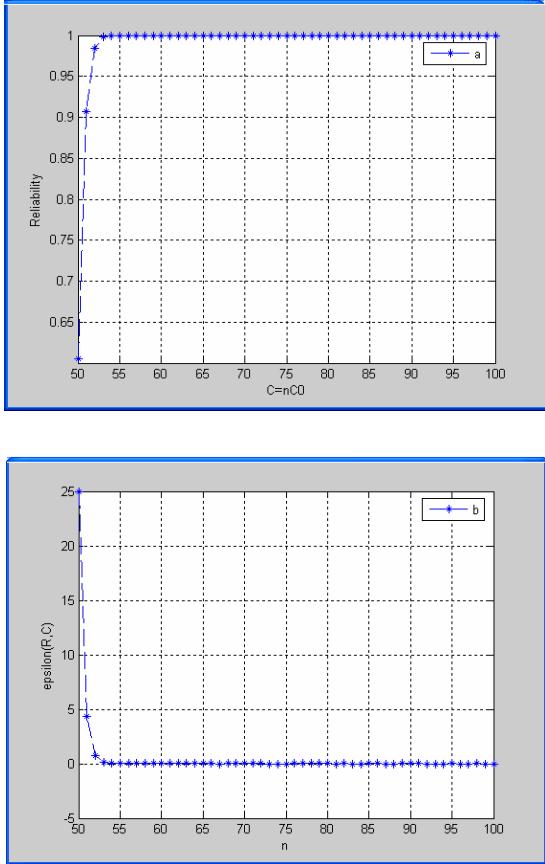


Fig. 3: Cost-reliability characterization of a 50-out-of- $n$ :G system with component reliabilities  $R_0 = 0.99$ .

$$(\Delta R)_{\Delta n=1} = [c(n+1, n+1)R_0^{n+1} + \sum_{m=k}^n (c(m, n+1)R_0^m(1-R_0)^{n+1-m} - c(m, n)R_0^m(1-R_0)^{n-m})]. \quad (10)$$

Using the binomial identifies

$$c(n+1, n+1) = 1, \quad (11)$$

$$c(m, n+1) - c(m, n) = c(m-1, n), \quad (12)$$

we reduce (10) to

$$(\Delta R)_{\Delta n=1} = R_0^{n+1} + \sum_{m=k}^n R_0^m(1-R_0)^{n-m}[c(m-1, n) - c(m, n+1)R_0], \quad (13)$$

and finally, obtain the cost elasticity of reliability as

$$\epsilon_{R,C} = \frac{n}{R} \left[ R_0^{n+1} + \sum_{m=k}^n R_0^m(1-R_0)^{n-m} c(m-1, n)(1 - \frac{n+1}{m} R_0) \right]. \quad (14)$$

Formula (8a) is a purely additive formula; it expresses  $R$  as the sum of nonnegative terms. Formula (14) is not an additive formula unless  $1 > \frac{n+1}{k} R_0$ ,

i.e., unless  $R_0 < \frac{k}{n+1}$ . Additive formulas have the distinguishing characteristic that they are less prone to the inaccuracies (and never subject to the catastrophic cancellation) caused by round-off errors.

Figures 2 and 3 present a cost-reliability characterization for a 50-out-of- $n$ :G system with component reliabilities  $R_0 = 0.8$  and  $R_0 = 0.99$ , respectively.

Formula (14) for the cost elasticity of reliability  $\epsilon_{R,C}$  gives satisfactory results up to  $R_0 = 0.8$  (Fig. 2(b)) and then starts to exhibit some unacceptable negative values (values of -0 rather than +0), i.e. it exhibits erratic behavior for very small or negligible values of  $\epsilon_{R,C}$  (Fig. 3(b)).

We must stress that the erratic behavior obtained is solely due to aggravated cumulative round-off error and is definitely not a result of some error in formulation or programming. Formula (14) gives acceptable and verifiable results for a wide range of values of  $k$ ,  $n$ , and  $R_0$ . However, it fails to assess  $\epsilon_{R,C}$  properly for systems having good components (i.e., for systems of practical interest). Anyhow, for such systems  $\epsilon_{R,C}$  diminishes and becomes indistinguishable from zero.

Equation (14) for  $\epsilon_{R,C}$  is obtained by using the smallest possible nonzero discrete increment  $\Delta n = 1$ . This increment is the best discrete increment since it is the nearest one to the "continuous" limit  $\Delta n \rightarrow 0$ . For a parallel system ( $k = 1$ ), we have two estimates for  $\epsilon_{R,C}$ , one based on the continuous limit  $\Delta n \rightarrow 0$  in equation (7) and another based on the best discrete increment  $\Delta n = 1$  in equation (14). Our computational experience reveals that there is no significant difference between these two estimates for large  $n$ , and small  $R_0$ , i.e. when (14) is not spoiled by accumulated round-off errors.

**Cost elasticity of MTTF for a  $k$ -out-of- $n$  system:** From cost considerations, MTTF seems to be a more tangible and cumulative measure than reliability itself.

Therefore, we introduce the concept of the cost elasticity of the MTTF, which we define as

$$\epsilon_{T,C} = \frac{(\Delta T / T)}{(\Delta C / C)} = \frac{(\Delta T / T)}{(\Delta n / n)}, \quad (15)$$

where

$$T = MTTF = \int_0^\infty R(t) dt. \quad (16)$$

For a  $k$ -out-of- $n$ :G system having components subject to a common constant failure rate (CFR)  $\lambda$ , the component reliability is

$$R_0(t) = e^{-\lambda t}, \quad t \geq 0, \quad (17)$$

and the MTTF of the system is obtained from equations (8b), (16), and (17) as

$$\begin{aligned} T &= \int_0^\infty \sum_{m=k}^n (-1)^{m-k} c(k-1, m-1) c(m, n) (e^{-\lambda t})^m dt, \\ &= \sum_{m=k}^n \frac{(-1)^{m-k}}{\lambda m} c(k-1, m-1) c(m, n). \end{aligned} \quad (18)$$

A simpler and a purely additive expression for  $T$ , however, can be obtained from the state diagram for a  $k$ -out-of- $n$ :G system [8]. When the system is in state  $m \geq k$ , it has  $m$  working components and it behaves exactly as a series system of a failure rate  $m\lambda$ . The system resides in this state for an average time ( $1/(m\lambda)$ ), and hence the MTTF of the system is

$$T = \frac{1}{\lambda} \sum_{m=k}^n \frac{1}{m}. \quad (19)$$

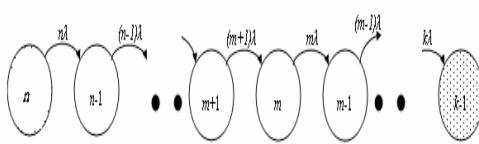


Fig. 4: State diagram for a  $k$ -out-of- $n$ :G system, in which each state is indexed by the number of working components, and the shaded state ( $k-1$ ) is one of catastrophic failure.

If we let the number of components  $n$  change to  $(n + \Delta n)$  in (19), then the MTTF changes to  $(T + \Delta T)$  given by

$$T + \Delta T = \frac{1}{\lambda} \sum_{m=k}^{n+\Delta n} \frac{1}{m}. \quad (20)$$

From (19) and (20), we can express the change  $\Delta T$  in MTTF due to a unit change  $\Delta n=1$  in the number of components as

$$(\Delta T)_{\Delta n=1} = \frac{1}{\lambda} \frac{1}{n+1}, \quad (21)$$

and hence, we can express  $\epsilon_{T,C}$  as

$$\begin{aligned} \epsilon_{T,C} &= \frac{\frac{1}{\lambda} \frac{1}{n+1} n}{\frac{1}{\lambda} \sum_{m=k}^n \frac{1}{m}} = \frac{\frac{n}{n+1}}{\sum_{m=k}^n \frac{1}{m}} \\ &= \frac{\frac{n}{n+1}}{\frac{1}{k} + \frac{1}{k+1} + \dots + \frac{1}{n-1} + \frac{1}{n}}. \end{aligned} \quad (22)$$

The cost elasticity  $\epsilon_{T,C}$  of the MTTF of a  $k$ -out-of- $n$ :G system is a function of  $n$  and  $k$  only and is independent of the component reliability  $R_0$  and the component failure rate  $\lambda$ .

Noting that the sum  $S = \sum_{m=k}^n \frac{1}{m}$  satisfies the following inequalities for  $k > 1$

$$S > \int_k^{n+1} \frac{dx}{x} = \ln\left(\frac{n+1}{k}\right), \quad (23)$$

$$S < \int_k^{n+1} \frac{dx}{x-1} = \ln\left(\frac{n}{k-1}\right), \quad (24)$$

we obtain the following tight bounds on  $\epsilon_{T,C}$

$$\frac{n/(n+1)}{\ln\left(\frac{n}{k-1}\right)} < \epsilon_{T,C} < \frac{n/(n+1)}{\ln\left(\frac{n+1}{k}\right)}. \quad (25)$$

## RESULTS

Table 1 lists  $\epsilon_{T,C}$  values in proper-fraction form (exact integer arithmetic) for small  $k$  and  $n$  values. Figures 5 and 6 represent the cost elasticity of MTTF for a parallel system and for a 50-out-of- $n$ :G system

Table 1: Value of  $\epsilon_{T,C}$  as a function of  $k$  and  $n$  for  $1 \leq k \leq n \leq 6$ .

$\frac{n}{k}$	1	2	3	4	5	6
1	$\frac{1}{2}$	$\frac{4}{9}$	$\frac{9}{22}$	$\frac{48}{125}$	$\frac{50}{137}$	$\frac{120}{343}$
2		$\frac{4}{3}$	$\frac{9}{10}$	$\frac{48}{65}$	$\frac{50}{77}$	$\frac{120}{203}$
3			$\frac{9}{4}$	$\frac{48}{35}$	$\frac{50}{47}$	$\frac{120}{133}$
4				$\frac{16}{5}$	$\frac{50}{27}$	$\frac{360}{259}$
5					$\frac{25}{6}$	$\frac{180}{77}$
6						$\frac{36}{7}$

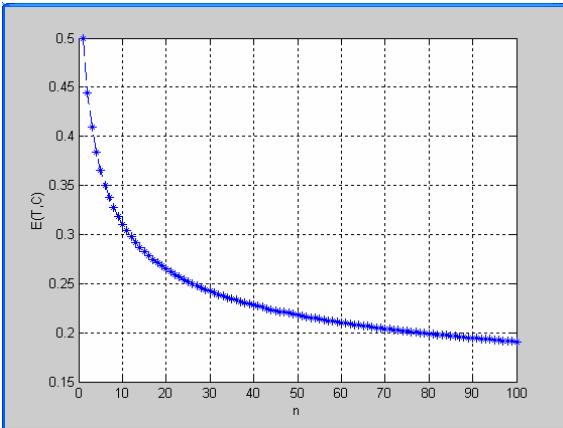


Fig. 5: Cost elasticity of MTTF for a parallel system versus its number of components  $n$ .

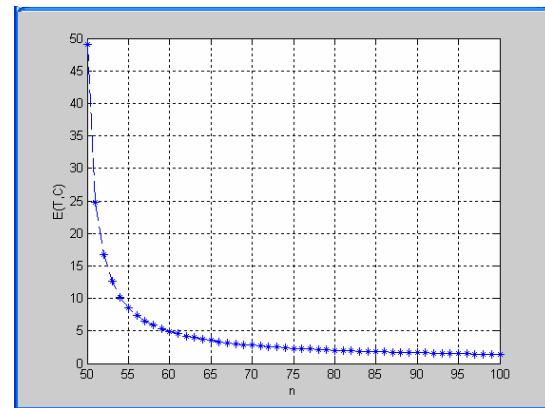


Fig. 6: Cost elasticity of MTTF for a 50-out-of- $n$ :G system versus its number of components  $n$ .

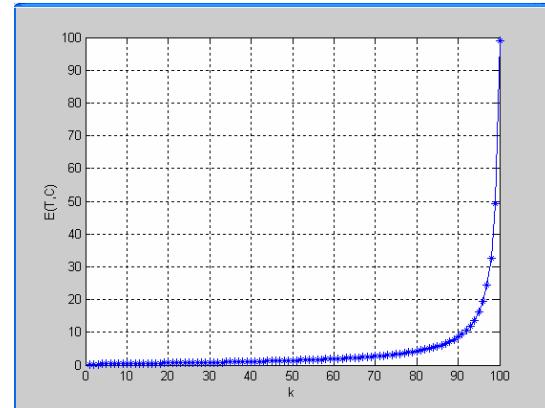


Fig. 7: Cost elasticity of MTTF for a  $k$ -out-of-100:G system versus the number of components  $k$  required for system success.

versus the number of components  $n$ . Figure 7 represents the cost elasticity of MTTF for a  $k$ -out-of-100:G system versus the number of components  $k$  required for system success. Table 1 and Figure 7 explain why the fail-safe (( $n-1$ )-out-of- $n$ :G system or 2-out-of- $n$ :F system) is so popular. Among redundancy systems it has the best cost for added redundancy since it has the highest  $\epsilon_{T,C}$ . Of course, the series system ( $n$ -out-of- $n$ :G system or 1-out-of- $n$ :F system) has an  $\epsilon_{T,C} = (n^2/(n+1))$  that is higher than that of the fail-safe system, but the series system has no redundancy at all and cannot tolerate even a single failure.

## DISCUSSION

The concept of cost elasticity of  $MTTF \in_{T,C}$  introduced herein is a novel concept and has several advantages when compared with the earlier competitive concept of cost elasticity of reliability  $\in_{R,C}$ . One advantage stems from the fact that the  $MTTF$  is a cumulative, integral, or averaging measure for reliability itself. For the wide class of  $k$ -out-of- $n$ :G(F) systems  $\in_{T,C}$  depends only on  $k$  and  $n$  while  $\in_{R,C}$  depends on component characteristics in addition to its dependence on  $k$  and  $n$ . For such systems, it was possible to express  $\in_{T,C}$  by a purely additive formula that is insensitive to round-off errors, while the  $\in_{R,C}$  formula is very susceptible to round-off errors to the extent that catastrophic cancellations take place. Moreover, the  $\in_{T,C}$  metric decreases but remains distinguishable from zero for large  $n$ , while the  $\in_{R,C}$  metric diminishes and becomes indistinguishable from zero for large  $n$  and  $R_0$ . This fact imposes a limitation on the utility of both metrics for large ultra-reliable systems.

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